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## Sensor Market Trends

International Frequency Sensor Association Publishing





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# IMU Market 2007-2012

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# Emerging MEMS 2010

Technologies & Markets 2010 Report

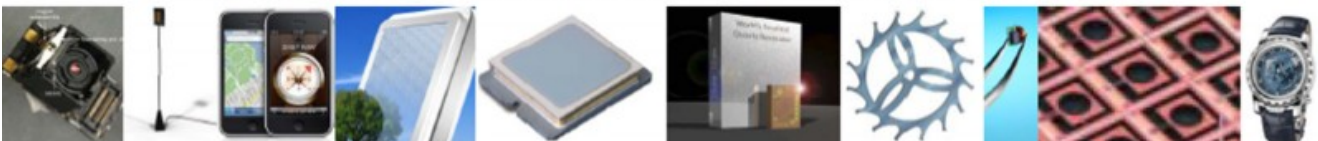
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May 22-27, 2011 - Venice, Italy



**Tracks:**

**A. Bioinformatics, chemoinformatics, neuroinformatics and applications**

- Bioinformatics
- Advanced biocomputation technologies
- Chemoinformatics
- Bioimaging
- Neuroinformatics

**B. Computational systems**

- Bio-ontologies and semantics
- Biocomputing
- Genetics
- Molecular and Cellular Biology
- Microbiology

**C. Biotechnologies and biomanufacturing**

- Fundamentals in biotechnologies
- Biodevices
- Biomedical technologies
- Biological technologies
- Biomanufacturing

**Important deadlines:**

Submission (full paper)	January 10, 2011
Notification	February 20, 2011
Registration	March 5, 2011
Camera ready	March 20, 2011

<http://www.iaia.org/conferences2011/BIOTECHNO11.html>



The Seventh International Conference  
on Networking and Services

## ICNS 2011

May 22-27, 2011 - Venice, Italy



**Important deadlines:**

Submission (full paper)	January 10, 2011
Notification	February 20, 2011
Registration	March 5, 2011
Camera ready	March 20, 2011

<http://www.iaia.org/conferences2011/ICNS11.html>

**Tracks:**

- ENCOT: Emerging Network Communications and Technologies
- COMAN: Network Control and Management
- SERVI: Multi-technology service deployment and assurance
- NGNUS: Next Generation Networks and Ubiquitous Services
- MPQSI: Multi Provider QoS/SLA Internetworking
- GRIDNS: Grid Networks and Services
- EDNA: Emergency Services and Disaster Recovery of Networks and Applications
- IPv6DFI: Deploying the Future Infrastructure
- IPDy: Internet Packet Dynamics
- GOBS: GRID over Optical Burst Switching Networks



The Sixth International Conference on Systems

## ICONS 2011

January 23-28, 2011 - St. Maarten,  
The Netherlands Antilles



**Important deadlines:**

Submission (full paper)	September 25, 2010
Notification	October 20, 2010
Registration	November 5, 2010
Camera ready	November 5, 2010

<http://www.iaia.org/conferences2011/ICONS11.html>

**Tracks:**

- Systems' theory and practice
- System engineering
- System instrumentation
- Embedded systems and systems-on-the-chip
- Target-oriented systems [emulation, simulation, prediction, etc.]
- Specialized systems [sensor-based, mobile, multimedia, biometrics, etc.]
- Validation systems
- Security and protection systems
- Advanced systems [expert, tutoring, self-adapting, interactive, etc.]
- Application-oriented systems [content, eHealth, radar, financial, vehicular, etc.]
- Safety in industrial systems
- Complex Systems

## Design of Piezoelectric PZT Cantilever for Actuator Application

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**Abstract:** Piezoelectric MEMS cantilever is used as a basic element in sensing and actuation. This paper proposes a structural design of MEMS cantilever for actuator application based on bulk MEMS micromachining technique. The structure consists of a silicon dioxide cantilever with an attached piezoelectric layer. The cantilever is designed using analytical modeling and simulation tool: CoventorWare2009. Analytical and simulation results demonstrate deflection of 5.9  $\mu\text{m}/\text{V}$  and 2.9  $\mu\text{m}/\text{V}$  respectively with a resonant frequency of 23 kHz. Obtained results are discussed and compared with the reported data. *Copyright © 2010 IFSA.*

**Keywords:** PZT, Actuators.

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### 1. Introduction

Ferroelectric thin films show great potential in the application area of electronics and opto-electronics due to their piezoelectric and pyroelectric properties. In the piezoelectric materials, energy conversion from electrical to mechanical domain and vice-versa; offer potential application in the field of sensors and actuators. Incorporation of piezoelectric materials in the current fabrication technologies is possible due to recent advances in thin film deposition.

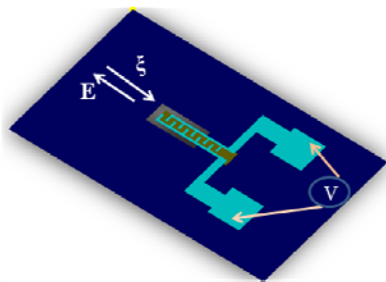
The range of piezoelectric materials like ZnO, AlN, polyimide, PVDF and PZT has been studied for their applications in MEMS field [1-3]. These materials, except PZT, have very low piezoelectric coefficient, thus their use is restricted in MEMS to certain extent. Many new materials like lead titanate (PT) lead zirconium titanate (PZT), lead magnesium niobate (PMN) etc. are the focus of interest worldwide. Lead zirconate titanate (PZT) is promising piezoelectric material having high piezoelectric coefficient which makes an attractive choice for MEMS application. Even though

material like PMN has higher piezoelectric coefficient, these material cannot be made in thin film form. PZT thin film deposition adds extra advantage of being processed along existing fabrication technology for batch device fabrication and thus preferred over other piezoelectric materials.

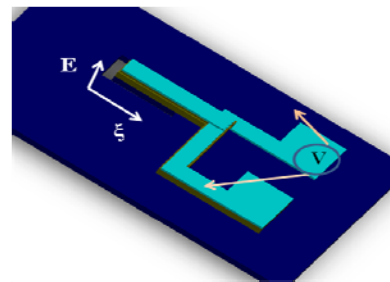
Piezoelectric PZT thin films are extensively used in the field of MEMS sensors and actuators due to its high piezoelectric and dielectric properties. A successful demonstration of PZT cantilever for application area such as, SPM/AFM cantilevers tip [4], accelerometer [5], touch button [6], chemical sensor [7], energy harvesting device [8] and RF switch [9] is reported. PZT cantilever shows promising applications in bio-sensing and is demonstrated by antibody-antigen detection and microfluidics [10-11].

A fix-free cantilever structure is chosen due to the higher deflection obtained. In-depth knowledge of piezoelectric behavior and cantilever modeling in order to design and develop PZT cantilever in certain applications is essential. Many theoretical models have been reported to explain the piezoelectric behavior of ferroelectric materials [12] and for piezoelectric cantilever modeling [13].

Piezoelectric based actuator use electric field induced strain including longitudinal, transversal and shear derived by the piezoelectric coefficient  $d_{33}$ ,  $d_{31}$  and  $d_{15}$  respectively. Depending upon the use of induced strain, two types such as  $d_{33}$  and  $d_{31}$  type PZT cantilevers are mainly used as shown in Fig. 1.1 and Fig. 1.2 respectively. The use of the shear coefficient for cantilever application adds trouble to fabricate devices and consequently not preferable.



**Fig 1.1.**  $d_{33}$  type cantilever.



**Fig 1.2.**  $d_{31}$  type cantilever.

In  $d_{33}$  type cantilever (see Fig. 1.1), in-plane electric field ( $E$ ) induces the in-plane strain ( $\xi$ ) contracting or expanding the PZT material, resulting into bending. This is generally achieved by using two metal interdigitated (IDT) electrodes on top of piezoelectric PZT thin film. In the second type ( $d_{31}$  type cantilever) (see Fig. 1.2), strain ( $\xi$ ) is induced normal to the applied electric field ( $E$ ). These induced strain, force PZT film to contract or expand and thus force cantilever to bend. This is generally achieved by sandwiching the piezoelectric PZT layer in two metal electrodes. In  $d_{33}$  type cantilever, PZT layer is partially covered by the metal IDT electrodes. PZT, not covered by metal electrodes suppress transverse displacement and generate stress concentration; which is undesired. In  $d_{31}$  type cantilever, as PZT layer is completely covered by the metal electrode, above mentioned problem is absent and thus  $d_{31}$  type cantilever based design is selected in this paper.

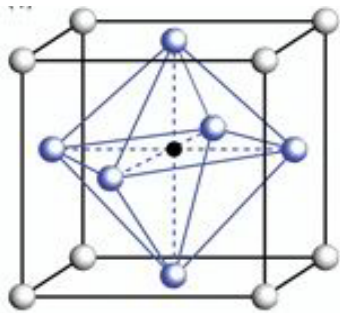
Cantilever displacement and resonating frequency is always a concern with the design. To achieve this, analytical modeling of PZT cantilever is presented in this paper. The piezoelectric PZT cantilever is modeled for actuation application using analytical calculations and its behavior is presented. Piezoelectric model is discussed on the basis of PZT crystal structure. The proposed design is simulated for applied electric field using finite element method (FEM) by 3D CoventorWare2009 software [14]. The analytical calculations are presented for cantilever deflection and resonant

frequency. The design is simulated for cantilever deflection, stress generated on cantilever and resonant frequency. Analytical and simulation results are discussed and compared with the reported data. Finally, the process of PZT cantilever beam fabrication is discussed.

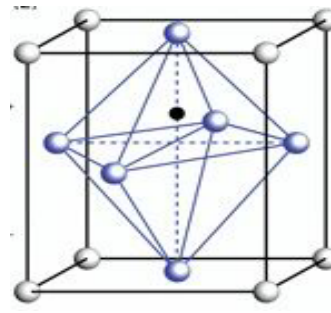
## 2. Modeling

PZT is a ferroelectric material which belongs to the  $ABO_3$  perovskite materials group. Basic cubic unit cell of PZT material is shown in the Fig. 2.1. Atom A (Pb in PZT case), B (Ti/Zr) and O (oxygen) are located at the corner, body center and face center position respectively. It is seen from Fig. 2.1 that, Zr/Ti atom is at the center of cube and structural symmetry is maintained.

When voltage is applied to the piezoelectric structure, bonding between body centers Ti/Zr atom and face center oxygen (O) atom gets disturbed, which causes asymmetry in structure. This shifting of center (Ti/Zr atom) causes strain in the material as shown in Fig. 2.2. This induced strain is relaxed by causing expansion or contraction of the material leading to mechanical deflection of the structure. This mechanism is smartly used in the MEMS cantilever for actuation.

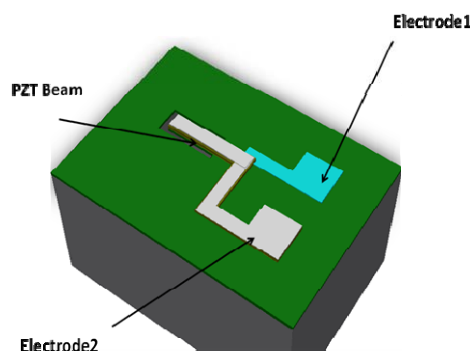


**Fig 2.1.** PZT structure.  $ABO_3$ .



**Fig 2.2.** PZT structure after center Ti/Zr displacement.

Using this piezoelectric material property,  $d_{31}$  type PZT cantilever is proposed for actuation application. The proposed structure of PZT cantilever is as shown in Fig. 3. The structure consists of silicon dioxide ( $SiO_2$ ) layer, used as a structural layer and PZT to convert electrical field in to mechanical displacement. Thin platinum (Pt) layer is used as an electrode material on both sides of the PZT thin film. The PZT cantilever is realized using silicon bulk micromachining (KOH) by forming v-groove. This technology was earlier used for fabrication of  $SiO_2$  cantilevers and can be used to fabricate PZT cantilever too [15].



**Fig. 3.** PZT beam structure.

## 2.1. Analytical Design

Applied electric field to piezoelectric film induces strain in the material, disturbing the structural geometry and forces to deflect. The relation between applied electric field (E) and electric displacement (D) is given by:

$$D = \epsilon_0 \epsilon_r E + dT, \quad (1)$$

where d is the piezoelectric coefficient; T is the stress and E is the relative dielectric permittivity.

The piezoelectric beam tip deflection in terms of physical dimensions of PZT cantilever is given:

$$d = \frac{t^3 d_{31} \left(\frac{V}{t_p}\right) (t_p + t_e) A_e E_e A_p E_p}{4(A_e E_e + A_p E_p)(E_p I_p + E_e I_e) + (t_e + t_p)^2 A_e E_e A_p E_p}, \quad (2)$$

where V is the applied voltage;  $A_i$  is the area of layer i;  $I_i$  is the moment of inertia of layer;  $d_{31}$  is the piezoelectric constant;  $E_i$  is the Young's modulus; d is the tip displacement;  $t_i$  is the layer thickness; e stands for elastic layer (SiO<sub>2</sub>) and p stands for piezoelectric (PZT) [16].

In addition to cantilever deflection, the natural resonance frequency of a two layer cantilever structure fixed on one end was calculated [12]

$$f = \frac{(1.875)^2}{2\pi L^2} \sqrt{\frac{(EI)}{w(\rho_e h_e + \rho_p h_p)}}, \quad (3)$$

where

$$(EI) = \frac{w}{12} \frac{(E_e h_e + E_p h_p)}{E_e^2 h_e^4 + E_p^2 h_p^4 + E_e E_p h_e h_p (4h_e^2 + 6h_e h_p + 4h_p^2)} \quad (4)$$

In these equations, E is the Young's modulus, I the moment of inertia, h the layer thickness, w is the width; L is the length of the cantilever and  $\rho$  the density respectively. Suffix e stands for elastic layer (SiO<sub>2</sub>) and p stands for piezoelectric (PZT). For the calculation, layer widths of silicon dioxide and PZT were kept equal. Therefore, the resonance frequency is independent of the cantilever width.

In proposed work, PZT layer is used as a piezoelectric and SiO<sub>2</sub> as the supporting layer. The material properties used in analytical calculation are shown in Table 1.

**Table 1.** Material property used for analytical modeling.

	Young's modulus	Piezoelectric coefficient ( $d_{31}$ )	Thickness (t)	Width (w)	density
<b>PZT</b>	70 Gpas	171	0.6 $\mu$ m	60 $\mu$ m	7.55 (g/cm <sup>3</sup> )
<b>SiO<sub>2</sub></b>	70 Gpas	-	0.85 $\mu$ m	60 $\mu$ m	2.3 (g/cm <sup>3</sup> )

Using equation (2) and material properties (see Table 1), the cantilever deflection was calculated for applied voltage of 1-10V for cantilever dimensions  $l = 200 \mu$ m,  $w = 60 \mu$ m and  $t = 0.6 \mu$ m.

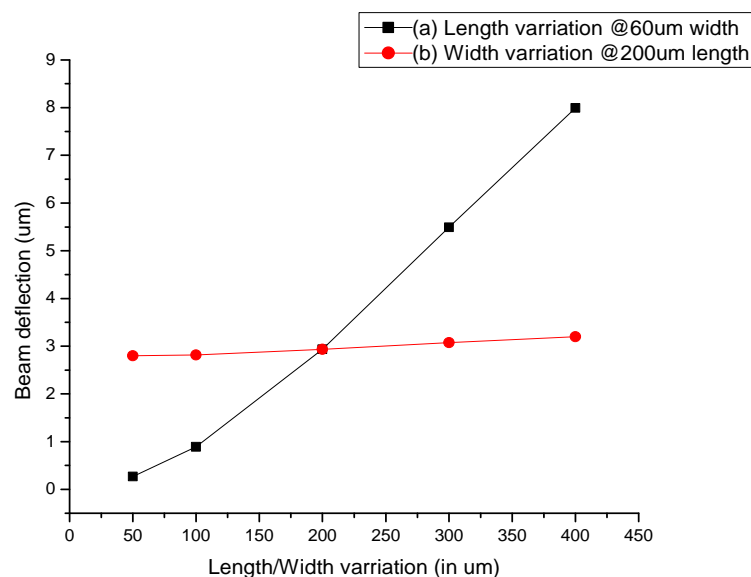
### 3. Simulation

The proposed PZT cantilever structure was simulated using CoventorWare2009 simulation tool. MEMMECH and CoSolve modules were used to find out the cantilever displacement in accord with applied voltage and its resonating frequency. In this paper, as PZT cantilever is proposed for application in RF MEMS structure; where up bending model is required thus simulation results for only up bending are presented.

#### 3.1. Physical Structure Optimization

For simulation of PZT based cantilever, optimization of physical dimensions was done by considering effect of various length, width and the fabrication parameters. Cantilever deflection behavior was studied by simulating PZT cantilever for various length and width by applying fixed voltage of 1 V. Effect of variation in cantilever length and width on PZT cantilever up bending is illustrated in Fig. 4. It could be seen from the figure that, cantilever deflection increases linearly with increase in the cantilever length. The deflection varies from 265 nm for 50  $\mu\text{m}$  to 7.99  $\mu\text{m}$  for 400  $\mu\text{m}$  long cantilevers. This trend is in good agreement with PZT cantilever modeling; as beam deflection is proportional to the cube of cantilever length ( $l^3$ ). An increase in length tends to decrease the resonant frequency of cantilever. Longer PZT cantilever are subjected to more curling during the fabrication process. Minimum tip deflection of 3  $\mu\text{m}$  is expected in the design at an applied voltage of 1 V and thus cantilever length was restricted to 200  $\mu\text{m}$ .

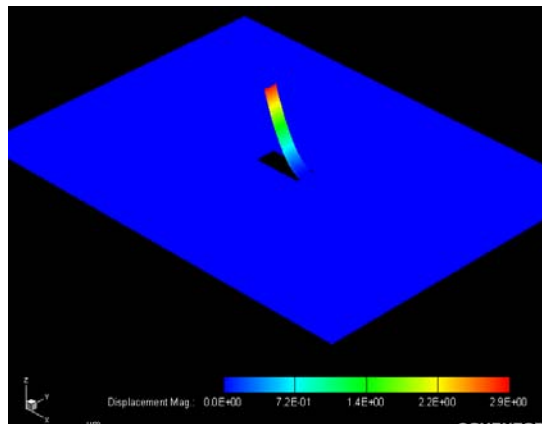
The variation in cantilever width is shown in curve (b) of Fig. 4. From this figure, it could be seen that, deflection of the cantilever was less sensitive to the width. The cantilever deflection changed from 2.8  $\mu\text{m}$  for 15  $\mu\text{m}$  wide beam to 3.19  $\mu\text{m}$  for 120  $\mu\text{m}$  width. In the cantilever fabrication process, wider cantilever will need longer processing time to realize in silicon bulk micromachining, and low width cantilever add extra burden in optimization of two Pt electrode contact pads. Thus, PZT cantilever width was optimized to 60  $\mu\text{m}$  in the present work. Considering the PZT processing steps, fabrication difficulties, PZT thin film cracking problem and required piezoelectric response, PZT thickness was optimized to 600 nm.



**Fig. 4.** Effect of cantilever length and width variation on beam deflection.

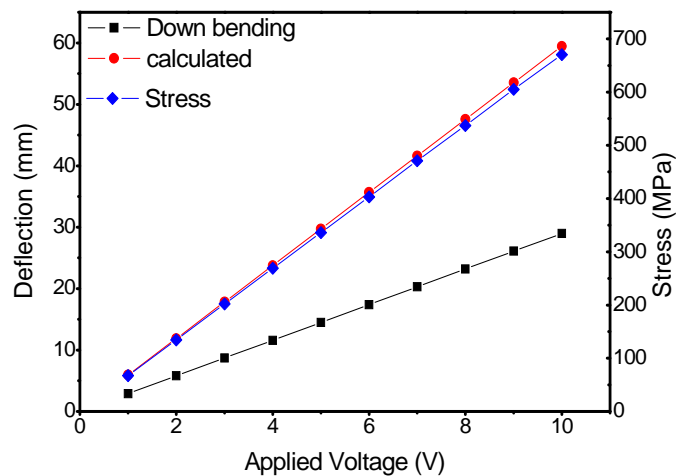
### 3.2. Deflection Due to Applied Voltage

Piezoelectric actuator response of the PZT cantilever was simulated by applying voltage to top and bottom electrodes and measuring deflection. From the simulated up bended model of PZT cantilever (see Fig. 5) one could derive that the deflection is higher at free end of the cantilever and zero deflection at the fixed end. Simulation and analytical calculation were carried down for up deflection of beam in accordance with the applied voltage range of 1-10 V.



**Fig. 5.** PZT cantilever up deflection.

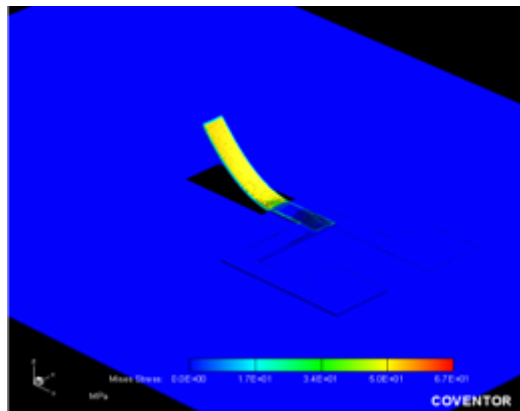
Obtained simulated and analytical results are plotted as shown in the Fig. 6. It could be observed that there is linear variation of tip deflection with respect to applied voltage. In analytical design, tip deflection was 5.9  $\mu\text{m}$  for 1 V applied, while maximum deflection of 59.4  $\mu\text{m}$  was observed for applied voltage of 10 V. Whereas CoventorWare simulation result shows that the PZT beam deflected for 2.9  $\mu\text{m}$  for applied voltage of 1V and maximum deflection of 26.4  $\mu\text{m}$  achieved for applied voltage of 10 V. This difference in analytical calculation and simulation results is attributed to increased structure thickness in simulation. In simulation two platinum layers of 150 nm were used as the electrodes. These layers increase the PZT beam stiffness and stiffer beam tends to deflect less.



**Fig. 6.** PZT beam deflection and stress variation against applied voltage.

Stress developed on PZT cantilever during up bending is in accordance with the applied voltage of 1-10 V (Fig. 6). Stress appeared on beam was 67 MPa for deflection of 2.9  $\mu\text{m}$ , which increase up to 670 MPa for the deflection of 26.4  $\mu\text{m}$ . The observed stress variation was linear with respect to up bending of the cantilever. As this design is proposed to actuate in 3-10  $\mu\text{m}$  range, the stress generated was 67-201 MPa.

Fig. 7 shows stress concentration along the PZT cantilever. It could be derived that, generated stress was concentrated at the fixed end. In case of PZT cantilever, when beam is deflected to 2.9  $\mu\text{m}$  deflection, the maximum stress of 67 MPa was at fixed end and 50 MPa was along the cantilever. This generated stress value is lower than the fracture limit of cantilever and thus this design is reliable for actuation application.



**Fig. 7.** Stress concentration on PZT cantilever.

In analytical design, if beam length changes to 500  $\mu\text{m}$ , then the calculated deflection was 37  $\mu\text{m}$ , which closely matches with the reported value of 34.7  $\mu\text{m}$  [12]. Analytical calculations are in accord with the reported deflection values of 3  $\mu\text{m}$  for 4 V [9]. The proposed structure deflects for 5.9  $\mu\text{m}$  for 1 V, which is best suitable for application in RF MEMS switches.

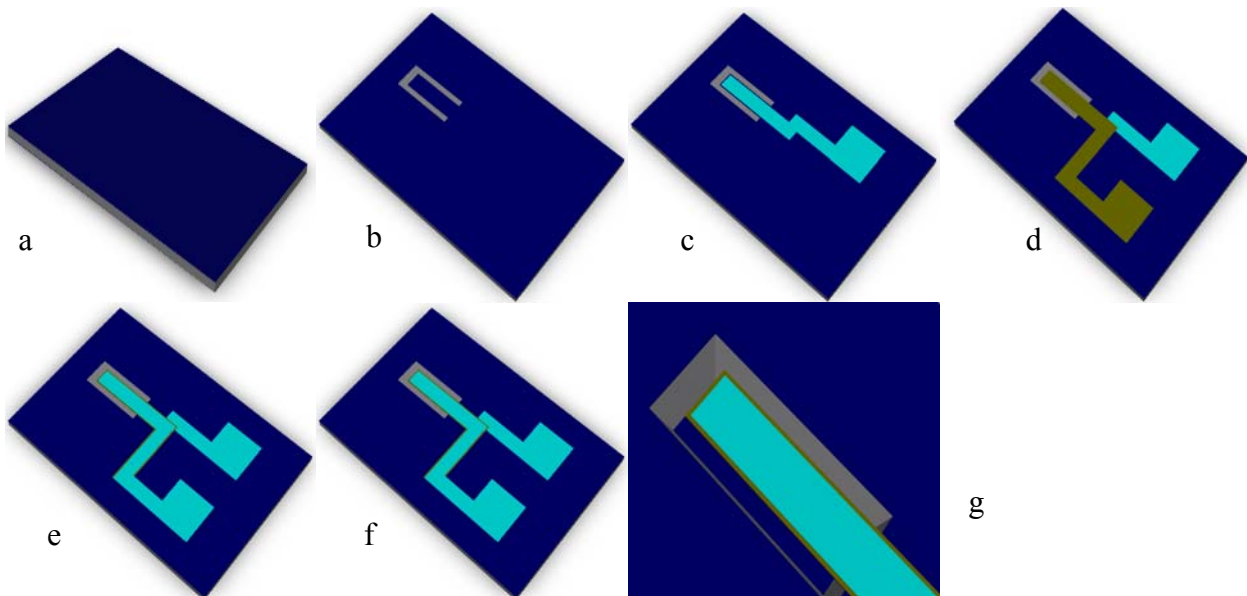
Analytically calculated resonant frequency of the structure was 22.15 KHz and that obtained from simulations using CoSolve simulator was 23 KHz. The lower value of resonating frequency is appreciated for small signal application along with lower actuation voltage [12]. The resonant frequency can be further lower down by increasing PZT layer thickness, with appropriate fabrication process consideration. These result shows that the proposed design with deflection of 2.9  $\mu\text{m}/\text{V}$  and resonating frequency of 23 KHz is well suited for small signal application and also for RF MEMS switch application.

#### **4. Fabrication Flow**

The proposed PZT cantilevers fabrication needs less fabrication time and reduce the use of critical process like deep reactive ion etching (DRIE) or use of very good masking materials like silicon nitride ( $\text{Si}_3\text{N}_4$ ) [8] and polymers masking material like polyvinyl difluoride (PVdF)/polytetrafluoro ethylene (PTFE) [17].

PZT based cantilever fabrication flow is proposed using silicon bulk micromachining. Starting with n type <100> silicon wafer, silicon dioxide layer of 800 nm is grown using thermal oxidation (Fig. 8.a). The oxide layer is patterned in order to expose underneath silicon material to etchant (Fig. 8.b). The

150 nm Pt layer is then sputter deposited and patterned to serve as a bottom electrode (Fig. 8.c). The titanium layer is used as adhesive layer prior to deposition of Pt layer. The 600 nm thin PZT is deposited on Pt surface using single target RF magnetron sputtering system. The sputtered PZT layer is patterned and annealed to obtain perovskite phase (Fig. 8.d). The 150 nm Pt layer is sputtered on PZT surface and patterned to serve as top electrode (Fig. 8.e). Finally the PZT cantilever is released using silicon bulk micromaching using KOH solution. The released PZT cantilever is shown in Fig. 8.f and close view of released PZT cantilever is shown in Fig. 8.g.



**Fig. 8 (a-g).** Fabrication flow of PZT based cantilever.

## 5. Conclusion

Piezoelectric PZT beam device is proposed for the actuation application. The proposed device shows deflection value of  $5.9 \mu\text{m}/\text{V}$  and simulated results show deflection of  $2.9 \mu\text{m}/\text{V}$ . The difference in yield is due to increase in stiffness of PZT cantilever with two Pt electrodes. Analytically calculated resonant frequency of the device is 22.1 kHz. The resonant frequency of the device is 23 kHz which is suitable for small signal application. Proposed device offers an easy fabrication method and is ideally suitable for low actuation voltage application as well as small signal application.

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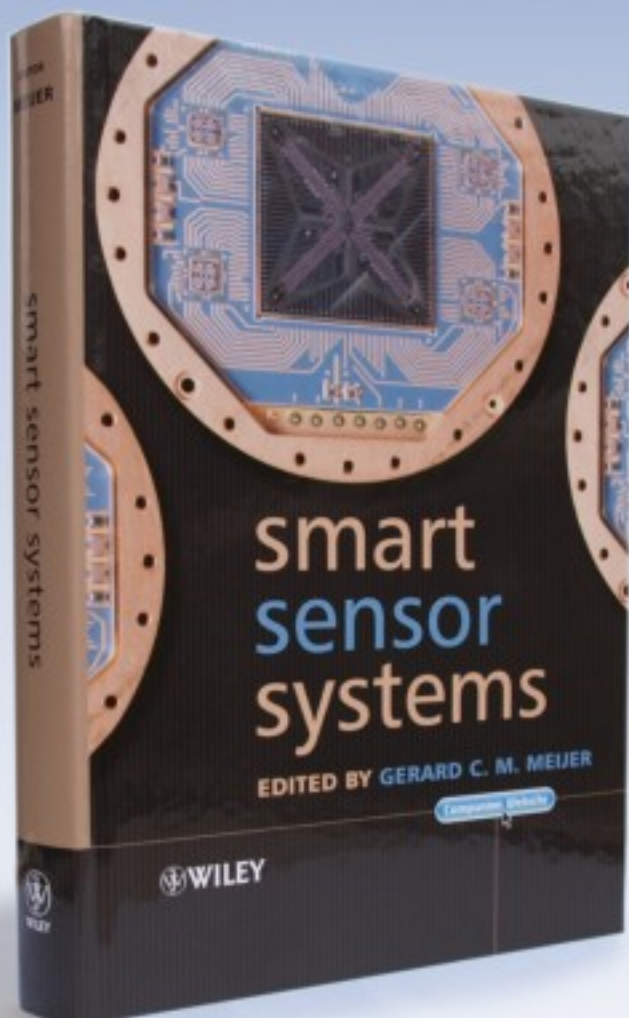
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