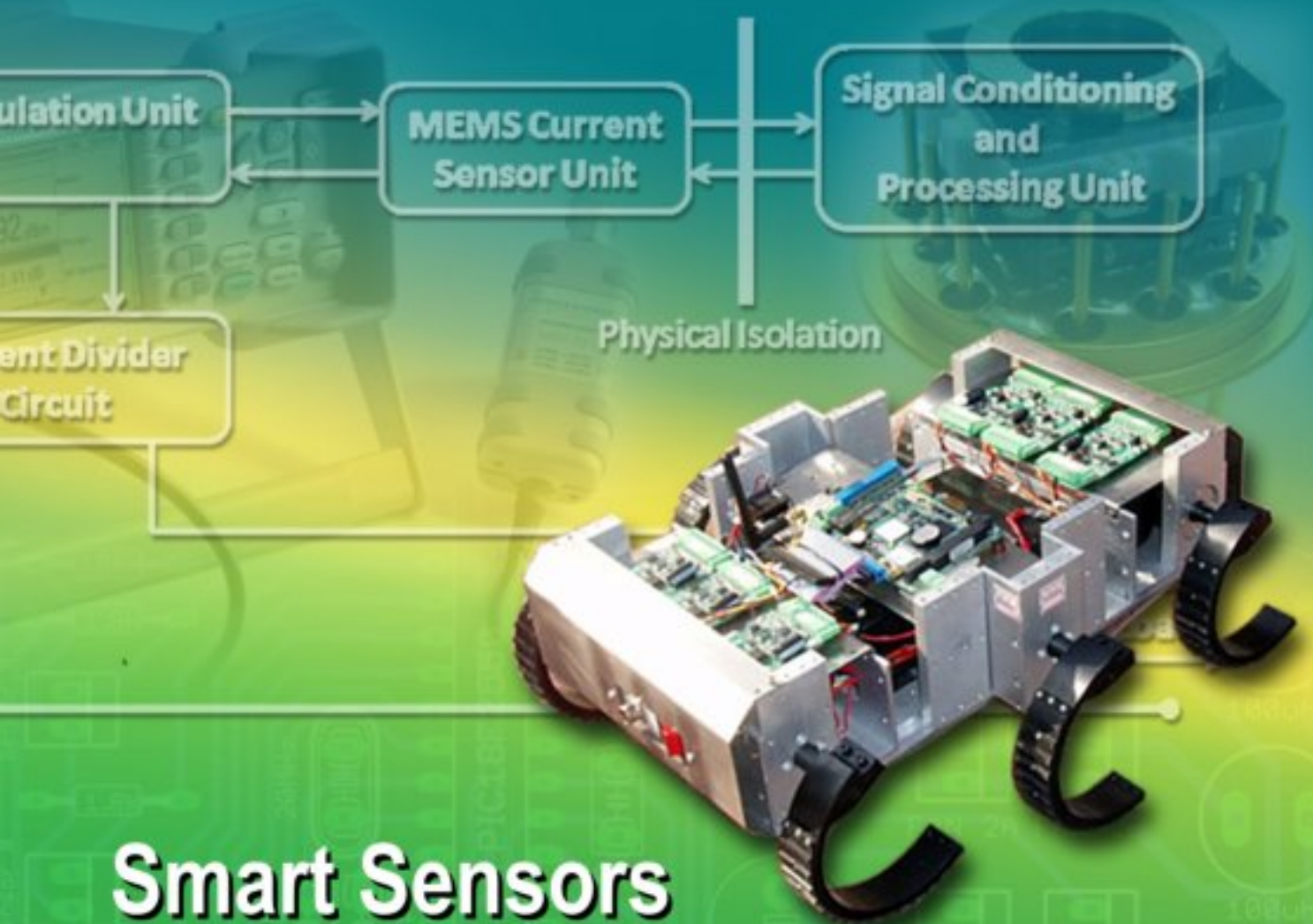


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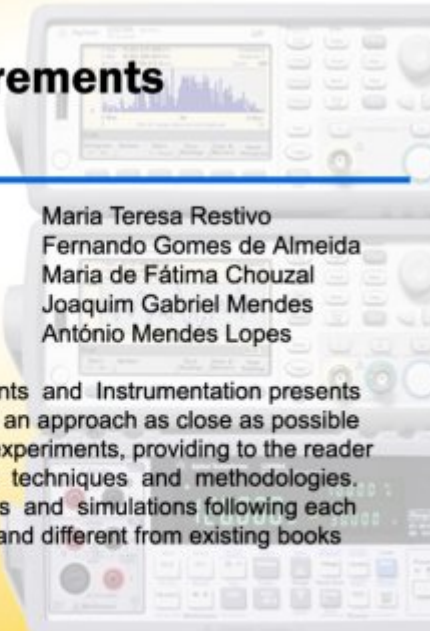





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Dynamic Control of Hexapod Robot Based on Plantar Pressure Sensor

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Abstract: This paper proposed a hexapod control method based on plantar pressure and designed the plantar pressure acquisition system. The experiments verified that the designed plantar pressure sensor can measure the dynamic plantar pressure accurately in real-time and the control method using plantar pressure can make the hexapod robot run stably with long time in different terrain condition.

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Keywords: Plantar pressure sensor, Hexapod robot, Dynamic control, Spring-loaded inverted pendulum.

1. Introduction

During the last decade there has been growing interest in the application of legged robot because the mobility of legged robots in the widest variety of terrain conditions is better than that of wheeled, tracked or railed robots. Hexapod robot is an important kind of legged robot which has the features of high energy efficiency and motion speed, for example, RHex can travel more than one body length per second based on autonomous energy [1].

Control method based on Bipedal Spring-Loaded Inverted Pendulum (BSLIP) is a dynamic control method of six legged robot, this control method force the true high dimensional system dynamics down onto the lower dimensional subspace corresponding to the BSLIP template. It improves substantially the maneuverability and dynamic range of six legged robot behaviors relative to the initial prototype open-loop algorithms [2]. The force of the system is acted through the legs which are on stance phase and it is the key to dynamic controller and it is often used to compute the states of legs and determine the boundaries of related two phases [3]. But how to acquire the force acted on the legs was not discussed in [2-4]. Considering all the force acted on the body is acted by legs and gravity, the gravity can be counted to a const, but the force acted by legs is related to time. If the force acted on legs acted by ground can be acquired, it will be helpful for the controlling of hexapod robot.

The goal of this paper is to design the plantar pressure sensor for measuring the force acted on the legs and design the dynamic controller based on BSLIP.

2. Hexapod Robot Model

2.1. The Structure of Hexapod Robot and Coordinates

The planar hexapod robot is depicted in Fig. 1, it consists of rigid body with six compliant legs, and each leg possessing only one independently actuated revolute degree of freedom. The attachment points of the legs are all fixed relative to the body symmetrically. The “virtual leg” is defined as the leg extending from the body center of mass to a stationary point on the ground [2]. The mass and inertia of the body are m and I respectively, the total mass of six legs $m_i \ll m$.

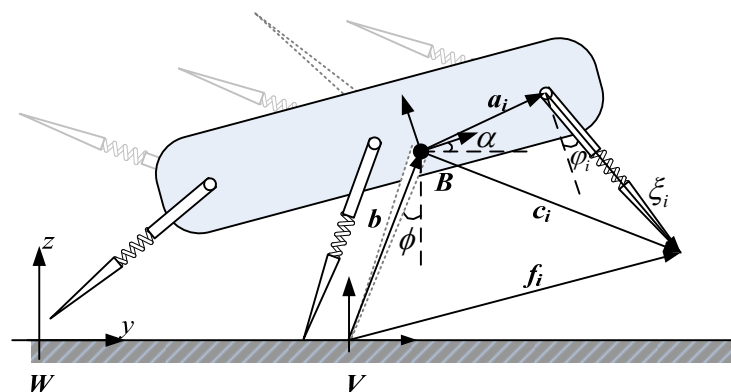


Fig. 1. Hexapod robot model.

We define three reference frame: W as the fixed inertial world frame, V as the virtual toe frame with the same orientation as W , but located at the foot of virtual leg, and finally B as the body frame, affixed to the center of the mass of the system. The position and orientation of the body are represented by a body-fixed frame B with respect to an inertial world frame W . The orientation of B determines the body pitch α and is also expressed by the rotation matrix ${}^W_B R$. The position of the body in V is denoted by b . The position of the toe is fixed on the ground and is denoted by f_i . Each leg is attached to the body through a pin joint with an independently controllable torque τ_i , located at a_i in the body coordinates B . Each leg is composed of a radial spring with stiffness k_i and incorporates viscous damping with coefficient d_i .

The toe position c_i defined with respect to V frame is:

$$c_i = f_i - b \quad (1)$$

If the toe position c_i is defined with respect to B frame:

$$c_i = a_i + \xi_i \quad (2)$$

Rotation matrix ${}^W_B R$ and ${}^B_W R$ are the functions of α :

$${}^W_B R = \begin{bmatrix} \cos \alpha & -\sin \alpha \\ \sin \alpha & \cos \alpha \end{bmatrix} \quad (3)$$

$${}^B_W R = {}^B_W R^T = \begin{bmatrix} \cos \alpha & \sin \alpha \\ -\sin \alpha & \cos \alpha \end{bmatrix} \quad (4)$$

According to B frame, ξ_i can be defined as:

$$\xi_i = {}^B_W R \cdot (f_i - b) - a_i = \begin{bmatrix} \cos \alpha & \sin \alpha \\ -\sin \alpha & \cos \alpha \end{bmatrix} \cdot \begin{bmatrix} f_{iy} - b_y \\ f_{iz} - b_z \end{bmatrix} - \begin{bmatrix} a_{iy} \\ a_{iz} \end{bmatrix} \quad (5)$$

Because a_i is a constant with respect to B frame, then we can obtain:

$$\dot{\xi}_i = \begin{bmatrix} -\sin \alpha & \cos \alpha \\ -\cos \alpha & -\sin \alpha \end{bmatrix} \cdot \begin{bmatrix} f_{iy} - b_y \\ f_{iz} - b_z \end{bmatrix} \dot{\alpha} + \begin{bmatrix} \cos \alpha & \sin \alpha \\ -\sin \alpha & \cos \alpha \end{bmatrix} \cdot \begin{bmatrix} \dot{f}_{iy} - \dot{b}_y \\ \dot{f}_{iz} - \dot{b}_z \end{bmatrix} \quad (6)$$

The polar coordinates of ξ_i is defined as:

$$\xi_i = [\rho_i \quad \varphi_i]^T = \left[\sqrt{\xi_{iy}^2 + \xi_{iz}^2} \quad \arctan(\xi_{iy} / \xi_{iz}) \right]^T \quad (7)$$

Derivative of ρ_i and φ_i with respect to time, we get:

$$\dot{\rho}_i = \frac{\xi_{iy} \dot{\xi}_{iy} + \xi_{iz} \dot{\xi}_{iz}}{\sqrt{\xi_{iy}^2 + \xi_{iz}^2}} \quad (8)$$

$$\dot{\varphi}_i = \frac{\xi_{iy} \dot{\xi}_{iz} - \xi_{iz} \dot{\xi}_{iy}}{\xi_{iy}^2 + \xi_{iz}^2} \quad (9)$$

2.2. Dynamic Equation

The configuration of the leg consists of stance phase and swing phase, in stance phase the leg contacts with the ground, in swing phase the leg does not contact with the ground. Six binary flags

$s_i \in \{0,1\}$ ($i = 1,2,\dots,6$) denote the leg configuration, 0 states that the leg touches the ground whereas 1 states that the leg is in flight.

The forces generated by the legs arise from their radial compliance and damping as well as the hip torques. The radial force component of i^{th} leg can be formulated as follows:

$$F_{ri} = -k_i(\rho_{i0} - \rho_i) - d_i\dot{\xi}_i, \quad (10)$$

where ρ_{i0} is the spring rest length of i^{th} leg.

As a result, i^{th} leg force acted on the ground can be written as:

$$F_i = {}^W_B R(\alpha + \varphi_i) \begin{bmatrix} \tau_i / \rho_i \\ -F_{ri} \end{bmatrix} = \begin{bmatrix} \cos(\alpha + \varphi_i) & -\sin(\alpha + \varphi_i) \\ \sin(\alpha + \varphi_i) & \cos(\alpha + \varphi_i) \end{bmatrix} \cdot \begin{bmatrix} \tau_i / \rho_i \\ -F_{ri} \end{bmatrix} \quad (11)$$

Where τ_i / ρ_i is the force component which is orthogonal to the radial orientation of leg.

Defining the force and torque vector acted on six legs:

$$F_r = [F_{r1}, \dots, F_{r6}] \quad (12)$$

$$\tau = [\tau_1, \dots, \tau_6] \quad (13)$$

Neglecting the Coriolis force and centrifugal force of the system, the dynamic equation of the system under the influence of external forces generated by the legs take the form:

$$m(\ddot{b} + g) = \sum_{i=1}^6 s_i F_i \quad (14)$$

$$I\ddot{\alpha} = \sum_{i=1}^6 s_i (f - b_i) \times F_i \quad (15)$$

Because the toe is fixed to the ground in the stance phase, the dynamic equation of the each leg is as the follow when neglecting the gravity:

$$m_i \ddot{f}_i = (1 - s_i) F_i = (1 - s_i) \cdot {}^W_B R(\alpha + \varphi_i) \cdot \begin{bmatrix} \tau_i / \rho_i \\ -F_{ri} \end{bmatrix} \quad (16)$$

3. Controller Based on BSLIP

3.1. Bipedal Spring-Loaded Inverted Pendulum (BSLIP) model

According to [3], in attempt to capture the characteristic features of the hexapod robot control we simplify the system to a Bipedal Spring-Loaded Inverted Pendulum (BSLIP) model, illustrated in Fig. 2.

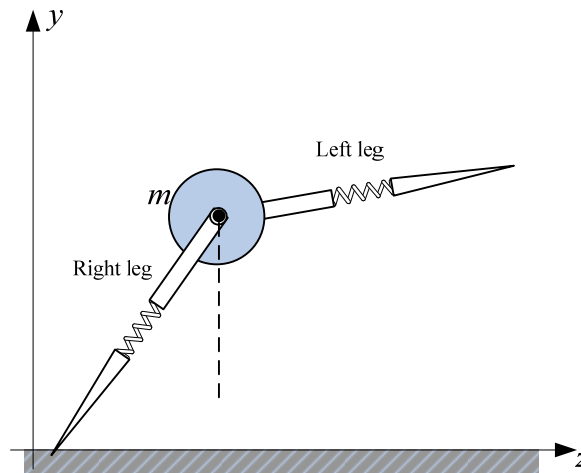


Fig. 2. BSLIP model.

The BSLIP model consists of a point mass m , attached to two compliant massless legs labeled as left and right which can freely rotate around the hip joint [3]. Each leg has two possible discrete modes: stance and swing. Throughout the stance phase of a leg its toe is fixed on the ground and the body is acted upon by the associated spring and damping forces. When the leg is in swing phase, it does not affect the body dynamics.

In the motion of hexapod robot, six legs are divided into two groups named left tripod and right tripod, the left tripod consist of front leg and rear leg in the left side and the middle leg in the right side of the body, the right tripod consist of the rest of legs. We assume that the left tripod and right tripod is always parallel during stance period and flight period. The two tripods are treated as the two virtual legs (Fig. 1) of the BSLIP model, so the control problem of hexapod can be treated as the control of the BSLIP model.

The BSLIP system has four modes: left stance, right stance, double stance and flight, determined by which legs are in contact with the ground. The dynamic characteristic of the system in different modes are different, and the control laws are different in different modes. How to identify the transitions between two modes is important, reference [3] and [4] use threshold functions respect to leg length and height of the body, the value of threshold functions determine the mode. But it is difficult to measure the height of the body in practice. We use the force \bar{F}_i ($i = 1, 2$) acted on the toe to identify the mode, then transitions between modes are governed by transition diagram illustrated in Fig. 3.

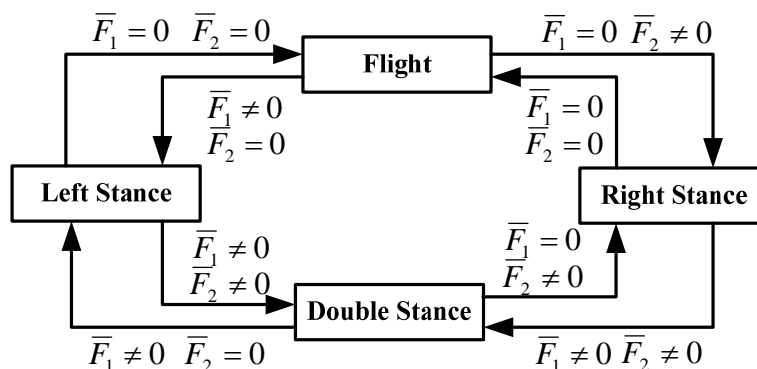


Fig. 3. Mode transition of BSLIP model.

3.2. Hexapod Robot Control Based on BSLIP Model

The design principle of the controller based on BSLIP for hexapod robot is to choose proper hip controls τ to bring the motion of the body as close as possible to the trajectories of the BSLIP [5]. Towards this end, the approach entails the followed separate components:

- (1) Imposing desired angles of two alternating tripods.
- (2) Determining the appropriate torque controls to tune the dynamics of the body during stance phase.
- (3) The coordination and control of the swing tripod.

The desired angles of two tripods is to ensure the stability of the tripod gait, we define the desired set of desired angles and times as:

$$\Phi^* = \{t_s^*, t_f^*, \varphi_s^*, \varphi_f^*\} \quad (17)$$

Where, t_s^* and t_f^* are the time when the leg is in stance phase and flight phase respectively, φ_s^* and φ_f^* are the angle of the leg when it is during the phase of stance and flight respectively.

Assume the actual angles and times as:

$$\Phi = \{t_s, t_f, \varphi_s, \varphi_f\} \quad (18)$$

The goal of the control is to acquire the torque of the hip to track the desired reference signal Φ^* . The errors of the angle during two phases are:

$$e_s = \varphi_s - \varphi_s^* \quad (19)$$

$$e_f = \varphi_f - \varphi_f^* \quad (20)$$

Proportional-derivative (PD) control algorithm is assigned to obtain the desired velocity to track the desired angle, the desired velocity take the form:

$$\omega_{sd} = k_{ps} e_s + k_{ds} \dot{e}_s \quad (21)$$

$$\omega_{fd} = k_{pf} e_f + k_{df} \dot{e}_f \quad (22)$$

Where proportional coefficient (k_{ps} and k_{pf}) and derivative coefficient (k_{ds} and k_{df}) values are determined by using the trial and error method.

During swing phase the torque acted on the leg can be determined by:

$$\tau_f = m_l \xi_0 \dot{\omega}_{fd} \quad (23)$$

The pitch α will be a const when the three legs in a tripod keeps parallel during stance period, then the dynamic equation is determined only by (14). Assuming that the actual force acted on the toe of the leg by ground is \bar{F}_r , then the length of the leg can be estimated by:

$$\hat{\xi} = \bar{F}_r / k \quad (24)$$

Form (14) we can derive the component orthogonal to the radial orientation of leg:

$$m(\ddot{b}_\tau + g_\tau) = F_\tau, \quad (25)$$

where $b_\tau = \hat{\xi} \cos \varphi$, $g_\tau = g \sin \phi = g \sin(\varphi - \alpha)$.

Then we can obtain the desired torque during stance phase:

$$\tau_s = m(\ddot{b}_{ad} + g_\tau)\hat{\xi}, \quad (26)$$

where b_{ad} is the desired height of the body, and it can be derived from the followed equation:

$$b_{ad} = \hat{\xi} \cos \varphi_{sd} = \frac{\bar{F}_r}{k} \cdot \cos \varphi_{sd} \quad (27)$$

The force \bar{F}_r is measured by force sensor fixed on the toe of the leg.

4. The Design of Force Sensor

The plantar pressure signal acquisition system consists of two parts: pressure sensor device, data acquisition circuit.

4.1. Collection of Sensor Model

The FlexiForce A201 Sensor was (Tekscan, Inc., USA) used to measure plantar pressure. Because the sensor is small, flexible and thin, the hexapod robot gait is not affected. The sensing area size of the sensor is 14 mm×14 mm×0.203 mm, and the pressure-sensitive area of the sensor is a 9.53-mm-diameter circle [6]. In the process of measurement the sensor's data was input to central control computer embedded in the robot through data acquisition card. Every sensor in different leg is numbered, so we can figure out the pressure of different leg through the sensors number. The sampling frequency can be set before experiment.

4.2. Design of Data Acquisition Circuit

Data acquisition circuit consists of signal condition circuit and signal acquisition model. The role of condition circuit is to transfer the current to voltage, we use surface mounted operational amplifier with low temperature drift and resistance in order to reduce the dimension of the device and improve the accuracy of the transition. The condition circuit is showed in Fig. 4, where R_1 is the sensor model with full-loaded resistance value 20 kΩ, R_2 is surface mounted resistance which resistance value is 20 kΩ, operational amplifier is MC34074 and its output is $V_{out} = 5V \times (\frac{R_2}{R_1})$. The voltage of the output is in the field of 0 ~ 5V. R_3 and C_3 is a low-pass filter to filter high frequency noise.

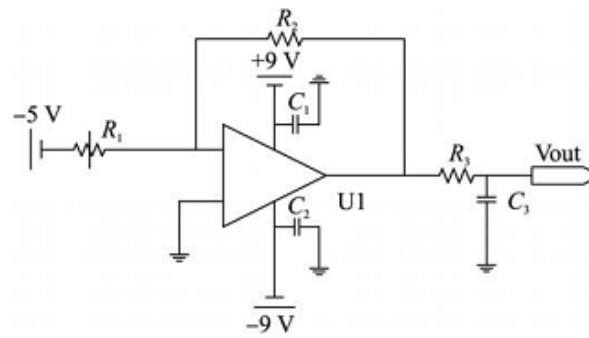


Fig. 4. Data acquisition circuit.

USB-4750 [7] (Advantech Inc., China) is used to acquire the output signal from data acquisition circuit.

4.3. Data Processing

The output of the force sensor device will be disturbed by noise, it is necessary to remove the noise from the data. The pressure signal during normal working is low-frequency signal and its amplitude is large, but the noise is high-frequency and its amplitude is small. Wavelet transform is a time-frequency analysis method [8], it has been widely used in the fields of signal denoising. In our experiments, we used Daubechie 4 (db4) wavelet, and the decomposition level was experimentally set to 4. Original data comparison with filtered data were showed in Fig. 5 (the blue line is original signal, and the red line is filtered signal). It is obvious that the noise has been filtered mostly.

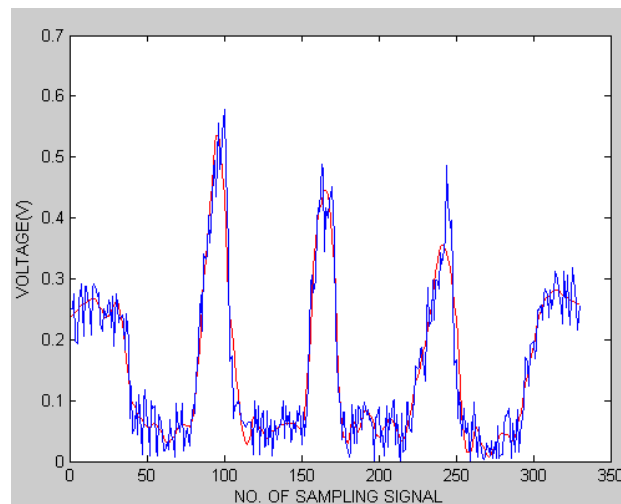


Fig. 5. Original data comparison with filtered data.

5. Experiment and Result

We designed a hexapod robot (see Fig. 6.), it consists of a rigid body and six C shaped legs. Each leg has a one revolute degree freedom and is driven by a DC motor. Power is provided by 24 V batteries. On-board computation is performed by a PC104 with 416 MHz running WinCE5.0 real-time OS. The control program is coded in Embedded Visual C4.0. The planar press sensor device is fixed on the toe of each leg.

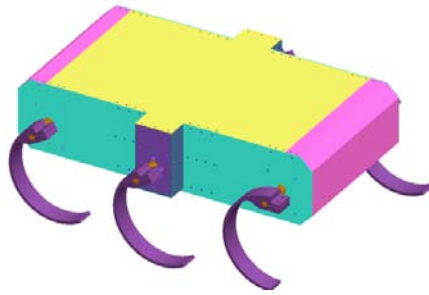


Fig. 6. Hexapod robot experiment platform.

The experiment was done in three types of terrain condition which are flat ground, grassplot and slope (see Fig. 7.). In order to compare the performance of the proposed control method we use two control methods, one is PD control method without force sensor and the other is proposed control method. The experimental results showed that the gait stability will deteriorate when the robot locomotion in long time especially in grassplot. But the locomotion performance improved largely used the proposed method, it can locomotion stably in long time in different terrain condition.

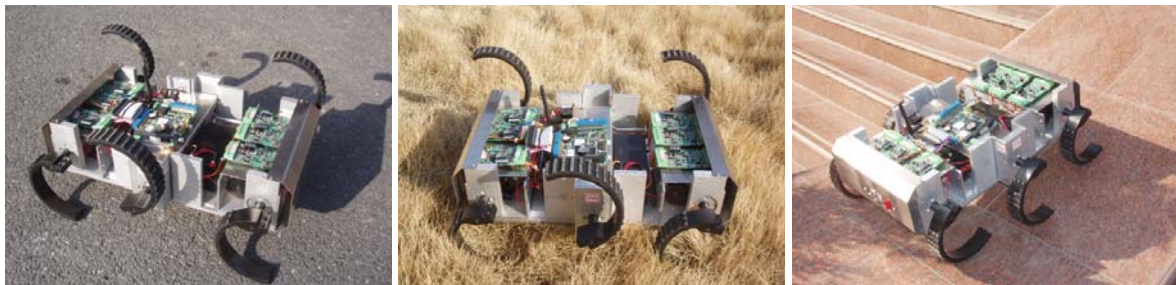


Fig. 7. Experiment of hexapod robot.

6. Conclusions

Hexapod robot has high locomotion performance comparing with wheeled and track robot. In this paper we proposed a novel control method based on planar pressure sensor. We designed the hexapod robot platform inspired by RHex and designed the planar pressure information acquisition system. The pressure collected from the sensor can be used to estimate the state of the robot and help to control the robot. Experimental results showed that the proposed method can make the hexapod robot locomotion stably in long time in different situation.

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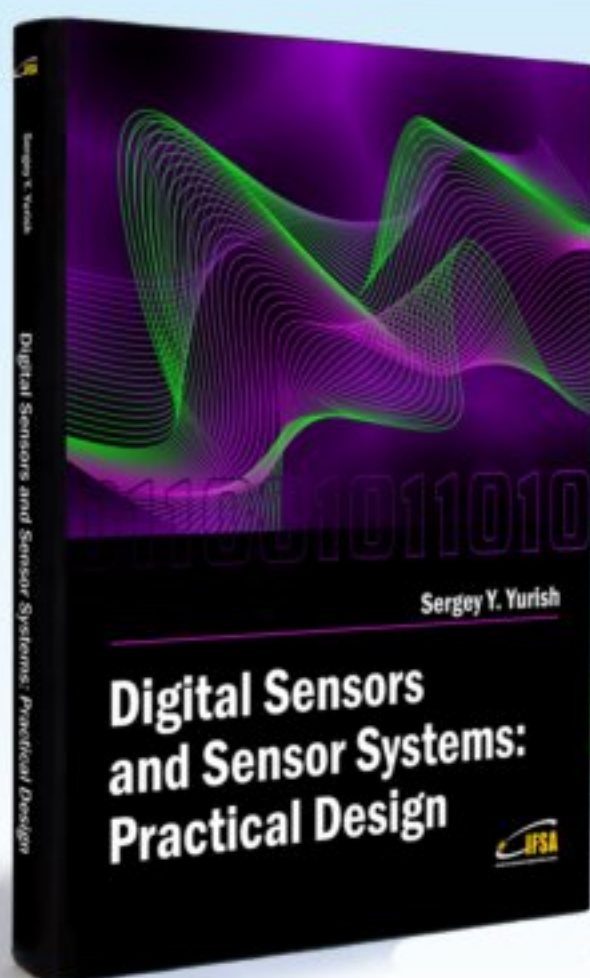
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