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Development of MEMS Varactor on Microwave Laminate Board for RF Applications

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Abstract: This paper presents the development of an electrostatically actuated MEMS varactor on microwave laminate board for RF MEMS applications using a convenient and economical fabrication approach. MEMS varactor is implemented using multilayer technology in which bottom electrode is patterned on microwave laminate board whereas beam structure and spacer (to create air gap) are realized using thin copper foil. Metal micromachining process is modified to attain straight beams on thin metal foil. A copper foil of 40 μ m thickness is used to realize beam structure. 15 μ m thickness copper foil is micromachined to form spacer. MEMS varactor is characterized for deflection and resonant frequency using Laser Doppler Vibrometer. Measured, analytically modelled and finite element method 3D tool Coventorware simulation pull-in voltages are 171 V, 153 V, 177 V respectively. Measured and FEM simulation pull-in voltage showed good agreement within 3.5 %. Measured and modelled capacitance tuning ratio is within 9.3 % which is acceptable. It is observed that measured resonant frequency is 2.8 kHz whereas modelled is 3.23 kHz which shows close agreement within 13.3 %. The proposed device has found major application in microwave and millimeter systems because microwave laminate board is the most preferred substrate for RF systems.
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Keywords: RF MEMS, Varactor, Microwave laminate, Milling, Micromachining, Photochemical.

1. Introduction

RF MEMS technology has poised to revolutionize communication system due to its advantages of low insertion loss, negligible DC power consumption and creating the feasibility of monolithic integrated

system. But in spite of its advantages, this technology is not being much used in commercial systems, the reason being its high cost and integration issues. Conventional RF MEMS fabrication needs high class clean room and sophisticated equipments which adds in the device cost. In addition to that, RF MEMS device fabricated on conventional substrates such as Si, Quartz, Glass etc. are packaged individually and are integrated in RF system using bonding techniques which may cause parasitics. Integration of individually fabricated and packaged RF MEMS device in system needs extra impedance matching circuitry which makes the system complex. These issues can be overcome by creating RF MEMS on microwave laminate board integrated with RF system i.e. monolithic RF system which is similar to system on chip.

Microwave laminate board is the most commonly used substrate for RF systems due to availability of wide range dielectric constant microwave laminate boards with low tangent loss. Since a decade, researchers are working on implementation of RF MEMS devices on microwave laminate board. RF MEMS switches [1, 2, 3, 4], phase shifter[5], monolithic phased antenna array with embedded RF MEMS phase shifter [6, 7] are already reported on microwave laminate board. In addition, fluidic microsystems [8, 9], MEMS capacitive pressure sensor[10] are also reported using PCB technology. There are fabrication processes reported to realize RF MEMS on microwave laminate board such as high density inductively coupled plasma chemical vapour deposition (HDICP CVD) which is a low temperature (90 °C -170 °C) process for microwave laminate board [11] and metal micromachining process using laser milling and computer numerical controlled (CNC) milling to realize RF MEMS membrane [4]. Still there is need to refine existing processes, in addition to the development of new fabrication approaches and processes to implement RF MEMS on microwave laminate board to cut down the cost and make fabrication processes commercially feasible.

In this paper we are demonstrating a low cost and convenient fabrication approach to realize MEMS varactor on microwave laminate board using modern PCB technology. Print and etch is used to pattern copper clad of microwave laminate board whereas micromachined thin metal foil is used to realize beam structure and spacer. This approach does not use any metal deposition/lithography/etching process. With the proposed approach, RF MEMS device can be implemented on microwave laminate board integrated in RF system. The major application of MEMS varactor is in distributed MEMS transmission lines which are already demonstrated to implement phase shifter and tunable filters. We reported meso-scale electrostatically actuated phase shifter on microwave laminate board (MEPL) [5] which operates similar to distributed MEMS transmission line phase shifter and also monolithic phased antenna array with embedded MEPL phase shifter [6].

MEMS varactor design aspects are discussed in section 2. Device fabrication and assembly are explained under section 3. In device fabrication approach, PCM (photo-chemical milling) process and conventional metal foil micromachining processes are described. Experimental set-up and measurement results are presented under section 4. Section 5 summarizes the major contribution of this research work.

2. Design of MEMS Varactor

This MEMS (Fig. 1) varactor is operated using electrostatic actuation mechanism. Electrostatic actuation takes place by applying DC bias voltage between beam and bottom electrode. Electrostatic force actuates the air bridge out of plane (along Z-axis), which causes change in capacitance. The electromechanical modelling is done to find out the actuation voltage for MEMS air bridge.

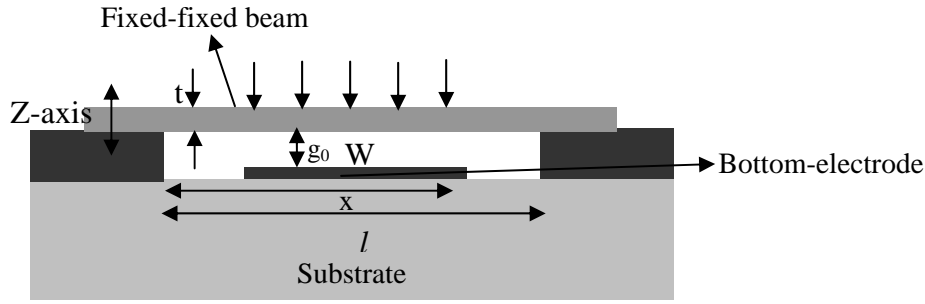


Fig. 1. Fixed –fixed beam with uniform load in the centre.

Electrostatic actuation is based on the Coulomb's law by which the electrostatic force (F_e) between oppositely charged plates separated by a gap g and a potential of V , is given by

$$F_e = \frac{1}{2} V^2 \frac{dC(g)}{dg} = -\frac{1}{2} \frac{\epsilon_0 w W V^2}{g^2}, \quad (1)$$

where the parallel plate capacitance C depends on the position of the movable bridge electrode whose width is w . The width of the bottom electrode is W . The beam is stable as long as the electrostatic force is balanced by the beam restoring force.

$$\frac{1}{2} \frac{\epsilon_0 w W V^2}{g^2} = k(g_0 - g) \quad (2)$$

Beam restoring force is the mechanical force due to beam stiffness k . In Eq. (2), g_0 is the original height of the beam electrode above the bottom conductor. Since the Coulomb force increases quadratically as g is reduced, electrostatic force dominates the elastic restoring force. Once the bias voltage exceeds a certain level, and the beam becomes unstable. This phenomenon is known as pull-in which occurs at around $g=1/3g_0$. For reliable operation of this phase shifter the deflection should be below this value. The corresponding bias voltage is given by

$$V_P = \sqrt{\frac{8kg_0^3}{27\epsilon_0 A}}, \quad (3)$$

where $A = w \times W$ is the actuation area (w is beam width and W is bottom electrode width). In this design, fixed-fixed beam is deflected with a uniformly distributed force directly above the center bottom electrode conductor trace [12]. Spring constant can be obtained from:

$$k = 32Ew \left(\frac{t}{L}\right)^3 \frac{1}{8\left(\frac{x}{L}\right)^3 - 20\left(\frac{x}{L}\right)^2 + 14\left(\frac{x}{L}\right) - 1}, \quad (4)$$

where E is Young's modulus of elasticity, t is the beam thickness, L is the beam length, k is spring constant of beam structure and x (from Fig. 1):

$$x = \frac{(L+W)}{2}$$

Resonant frequency of the beam structure is given by the following expression:

$$f_r = \frac{1}{2\pi} \sqrt{\frac{k}{m}} \quad (5)$$

where m is mass of beam which can be evaluated using beam material density and volume. Young's modulus of copper is taken 128GPa. Air gap is selected depending on the availability of copper foil thicknesses whereas beam thickness is decided under consideration of manual handling during fabrication. Other design parameters are selected with the help of analytical model. The finalized design parameters of the MEMS varactor are listed in Table 1.

Table 1. Design parameters of the fabricated device.

Design parameter	Value
Beam thickness (μm)	40
Beam length (μm)	6000
Beam width (μm)	300
Bottom electrode width (μm)	4000
Air gap (μm)	15
Young's Modulus (GPa)	128

The analytically modelled pull-in voltage obtained using equation (3) is 153 V. But, this expression for pull-in voltage assumes 1-dimensional beam movement and deformed beam without considering torsion. It considers only parallel plate capacitance without fringing effects. Fringing effect is due to the fields at the edges. Therefore 3D simulation are carried out in Coventorware which is a finite element method based electromechanical simulation software, for an accurate modelling incorporating the effects which were not included in the analytical approach. Coventor simulation pull-in voltage is 171 V. Analytically modelled and FEM 3D Coventorware simulation pull-in voltage is within 10.5 % which is acceptable. The device with design parameters listed in Table 1 is fabricated and characterized. Device fabrication details are discussed in next section.

3. Fabrication of MEMS Varactor

A thin copper foil is used to form top beam structure membrane as well as spacer layer to create the air gap between beam and bottom electrode. Air gap equal to metal foil thickness is created by inserting metal foil spacer between beams and bottom electrode. Beams and spacer are patterned on copper foil using photochemical milling. Bottom electrode conductor traces are patterned on microwave laminate copper clad using 'print and etch'. Beam structures membrane is attached to microwave laminate metal clad with spacer metal in between. In order to minimize the fabrication cost, no metal deposition/lithography/etching is used. Fabrication processes are modified to meet these challenges during fabrication of MEMS varactor on microwave laminate board.

3.1. Patterning Copper Clad of Microwave Laminate Board

Microwave laminate board Arlon AD250 of height 60mils with dielectric constant 2.5 is used as substrate. Microwave laminate board cleaning is done by soft rubbing with scrub and giving 1min dip in 10 % Sulphuric acid (H_2SO_4) solution. After this, the sample is thoroughly washed with the DI water to remove the acid contents and kept in the oven for 5min at 80 °C temperature to dehydrate water

contents from microwave laminate board. The cleaning process removes organic particles, dust and other external particles from the substrate surface. Microwave laminate board with both side metallization layers as shown in schematic Fig. 2 (a), is cleaned to pattern the bottom electrode and ground conductor traces of MEMS varactor. Here dry film photo-resist is laminated and exposed for lithography on the microwave laminate board. Print and etch technique is used to realize conductor traces on one side and conductor clad is completely etched away from the other side of microwave laminate board, as shown in schematic Fig. 2 (b). Width of the bottom electrode conductor trace is 4000 μm , whereas the slot spacing between centre conductor and side conductor is 1000 μm .

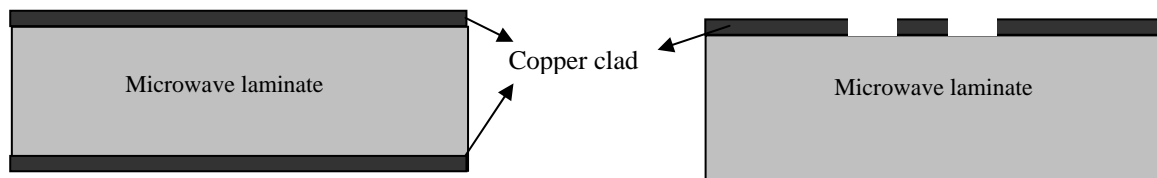


Fig. 2. (a) Microwave laminate board with both side metallization; (b) CPW patterned on the microwave laminate board

3.2. Copper Foil Micromachining to Create Beam Structures

Copper foil of 40 μm thickness foil is used as membrane to realize beam structures. In conventional MEMS microfabrication, metal patterning is carried out using wet chemical etching or dry etching whereas Ramadoss et al [4] reported CNC/laser milling to pattern films to implement MEMS on PCB. Initially, attempts were made to patterns copper foil using wet chemical etching. In wet chemical etching, sample is dipped in wet etchant and kept still. Beam structures realized using wet chemical etching resulted in wrinkled beam structures (Fig. 3). Fig. 4 is 3D image of beam structures taken with Wyco profilometer which depicts that surface profile variation of patterned beam structure is 64 μm to 212 μm along Z-axis. Wrinkles in beam structures are due to internal residual stresses of the foil. Measured residual stress of 40 μm thick copper foil is $\sim 74\text{MPa}$. Therefore internal residual stress of the copper foil should be managed to achieve straight beam structures which is possible using photochemical milling (PCM).

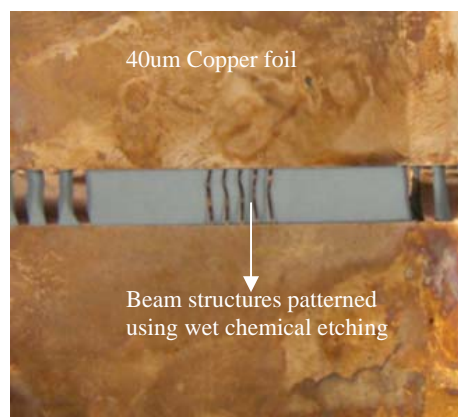


Fig. 3. Multiple beam structures patterned on copper foil using wet chemical etching.

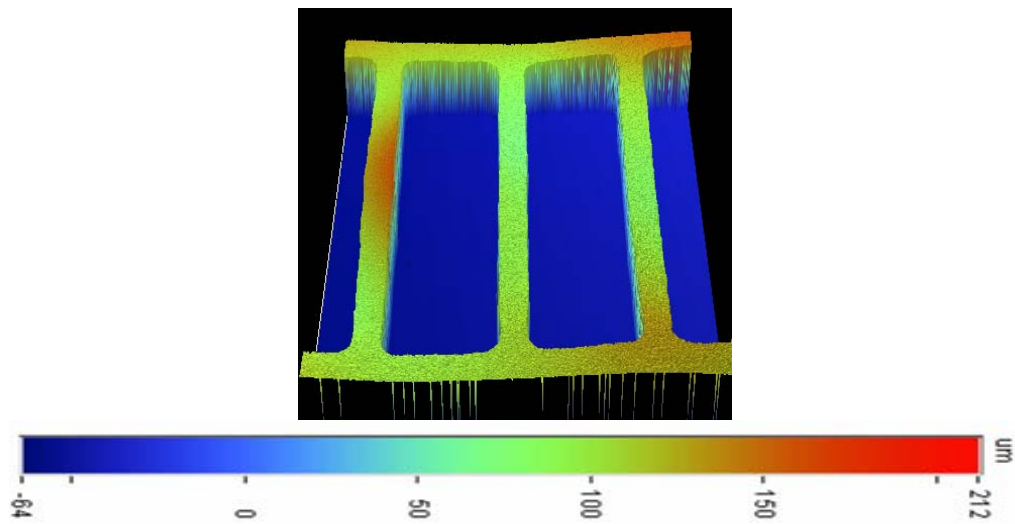


Fig. 4. Wyco optical profilometer 3D images of beams patterned on copper foil using wet chemical etching.

3.2.1. Photochemical Milling (PCM)

To remove the effect of induced residual stress on beam structures during copper foil micromachining, a modified technique photochemical milling is proposed. In PCM, etching is done with chemical etchants under controlled temperature and pressure of etchants. In this, etching line consist of multi-chambered machine that has driven-wheel conveyors to move the plates and arrays of spray nozzles above and below the plates. The etchant is an aqueous solution of acid that is heated and directed under the pressure on both sides of the plate. The etchant reacts with the unprotected metal essentially corroding it away quickly. After neutralizing and rinsing, the remaining part of resist is removed and metal foil is cleaned and dried. It can be used for materials of thicknesses ranging up to 200 μm . Metals that can be patterned include aluminium, brass, copper, manganese, nickel, silver, steel, stainless steel, zinc and titanium. Etching is controlled by varying pressure, temperature, spray system, etchant concentration, or distance between object and nozzle [13].

Copper foil of 40 μm thickness is used to create beam structures membrane. Copper foil is cleaned by soft rubbing with scotch and 1min dip in 10 % Sulphuric acid. Copper foil is laminated on both sides and structures are patterned on dry photoresist using lithography. Ferric chloride or cupric chloride solutions can be used for copper foil micromachining with PCM. The constituents for cupric chloride etchant are 10 % hydrochloric acid and 3 % hydrogen peroxide in 100 gm/lit cupric chloride. Whereas additives for ferric chloride solution are 10 % hydrochloric acid and 300 gm/lit ferric chloride. Here we used cupric chloride solution as etchant because it is more suitable to get better side walls of copper foil and recycling of the solution is possible. Ferric chloride solution will cause more sludge formation and hence can not be recycled. Ferric chloride may be better etchant for stainless steel like metals. There are varieties of spray bank system such as fish tail, flower type, cone type etc. Here we used wide range of fish tail type spray system which covers wide length of 6 inches wafer. There are two possible ways of etching 1) etching on both side top and bottom and 2) single side only from top or bottom. Single side etching can be used for foils of thickness up to 10 μm and its better to use double sided etching for thick copper foils of >10 μm because single side etching may cause under-etching for thick foils >10 μm . Here we used double sided etching as copper foil is >10 μm . Etching is done at temperature of 40 degree under 10 Psi pressure. PCM process flow is presented in Fig. 5. The spacing between consecutive beams can be obtained 1.25 times the foil thickness. PCM created the feasibility of achieving straight beams by controlling the residual stress induction in the etched areas as shown in Fig. 6. PCM patterned beams investigations are made to visualize the beam straightness with Wyco profilometer. 3D images of Wyco profilometer (Fig. 7) shows that beams are at the same level along

Z-axis without any crumbling with variation of ± 300 nm. Experienced pull-in voltage of demonstrated MEMS varactor is 177V which is comparable to MEMS based electronically steerable antenna reported in [7]. It is closely observed that PCM patterned beams are with very fine etched side walls, as shown in microscopic image (Fig. 8).

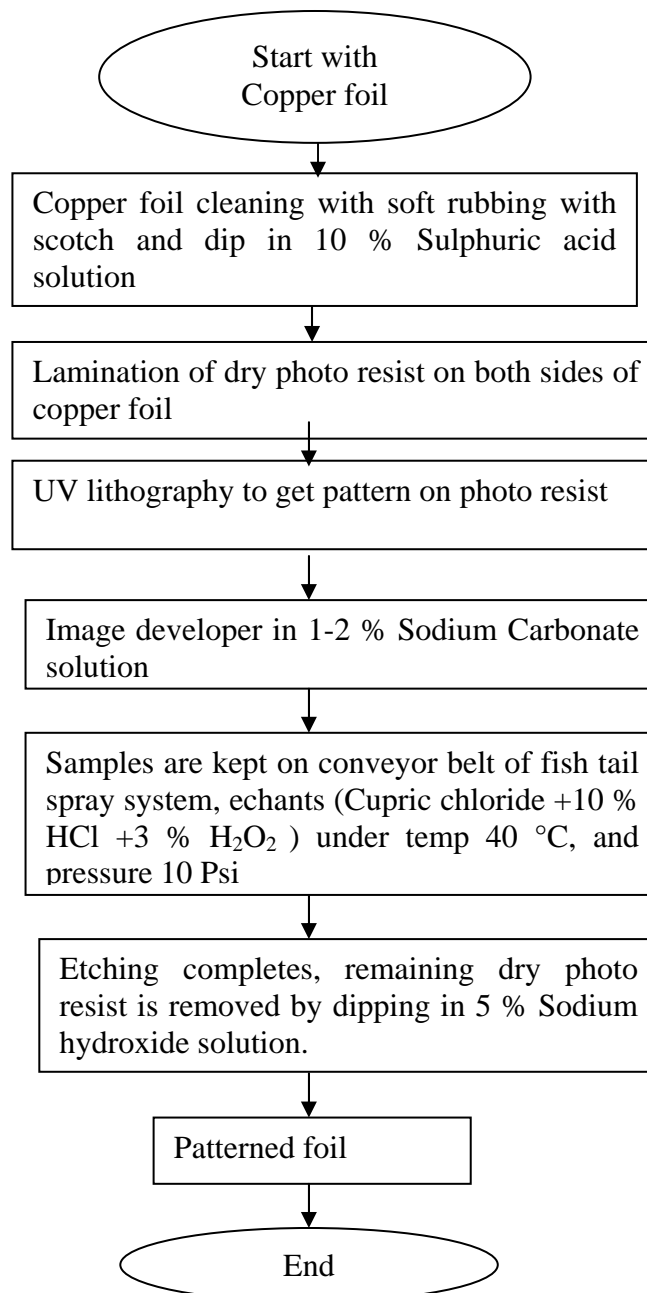


Fig. 5. Photo-chemical milling process steps followed to pattern copper foil.

3.3. Spacer Formation

Copper foil of 15 μm thickness is used to define the air gap between beam structures membrane and bottom electrode. Spacer is formed by photochemical milling (PCM) of the copper foil. Top view of spacer realized by patterning 15 μm copper foil using PCM is shown in Fig. 9. Length by width of spacer is 20 mm \times 10 mm.

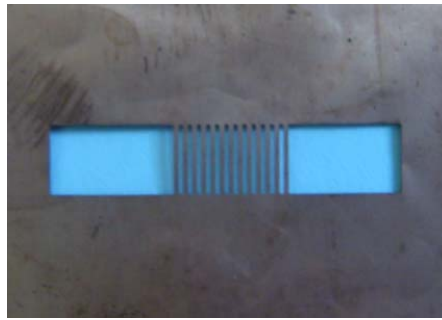


Fig. 6. Multiple bridge structures patterned on copper foil using photochemical milling.

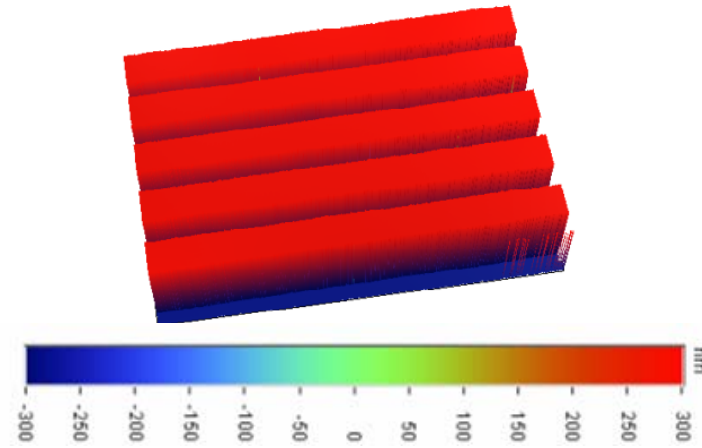


Fig. 7. Wyco optical profilometer 3D images of beam patterned on copper foil using PCM.

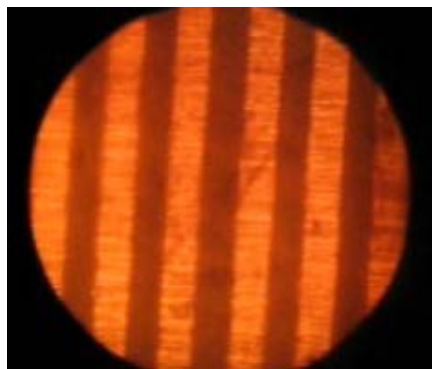


Fig. 8. Microscope images of the beam patterned on copper foil using.

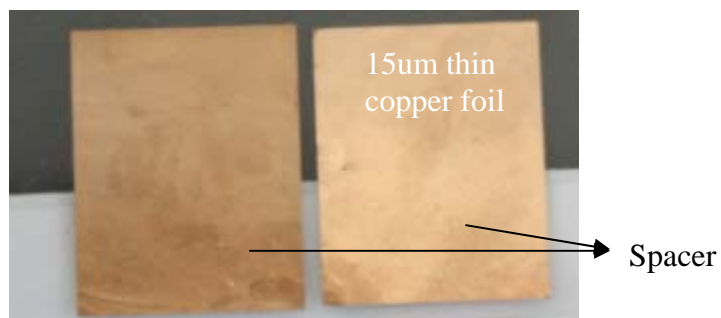


Fig. 9. Spacer realized in 15um thin copper foil.

3.4. Assembly of MEMS Varactor

Microwave laminate board with patterned conductor traces, spacer, and beam structures are assembled along with a glass/plexi-glass on top and bottom to realize the MEMS varactor as shown in Fig. 10. Glass/plexiglass is used at the top of the configuration for the protection as well as to maintain the straightness of the beam structures realized on the copper foil. In this multilayer assembled MEMS varactor, base material of the microwave laminate board and topmost plexiglass/glass (thickness 2mm) acts as the top and the bottom package layers respectively. Fig. 11 is photograph of MEMS varactor fabricated on microwave laminate. Although the final assembled device is completely covered with the plexi-glass to protect the bridges, samples prepared specifically for the electromechanical characterizations are assembled with the top plexi-glass having cavity to make direct contact of the laser beam of the LDV and the beam structure. LDV measurements of the device with glass along bridge may cause inaccuracy in the measurements due to multiple reflecting surfaces.

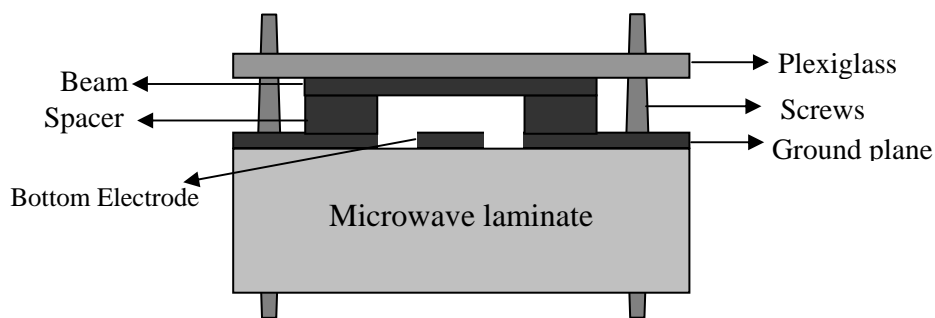


Fig. 10. Cross-sectional view of assembled MEMS varactor.



Fig. 11. Assembled MEMS varactor.

4. Measured Results

Laser Doppler Vibrometer (LDV), which is based on the principle of Doppler effect, is used for beam deflection and resonant frequency measurements. Fig. 12 shows the experimental set-up to perform the electro-mechanical characterization of the MEMS varactor. The laser beam of the LDV is focused on the beam structures of the device through the cavity made in plexi-glass for measurements. AC (peak to peak 10 V) plus variable DC bias is applied across bottom centre electrode and air bridge. Measured deflection and resonant frequency characteristics are discussed next.

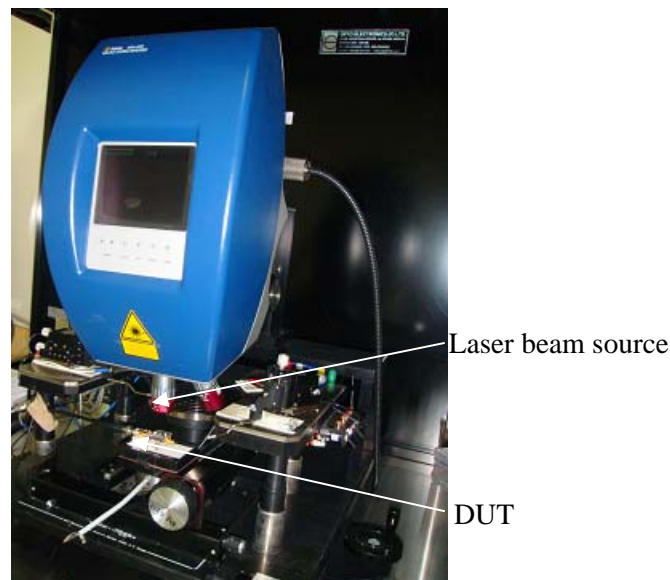


Fig. 12. Lased Doppler Vibrometer set up for the electromechanical testing.

4.1. DC Bias Voltage vs. Displacement Measurements

Electromechanical characterization of MEMS varactor is performed to measure deflection variation on applying DC bias voltage. Beam displacement is noted on increasing the DC bias voltage in steps which is shown in Fig. 13. Variation of capacitance with voltage is also shown in the same plot where capacitance is evaluated from the displacement. Measured pull-in voltage is 177 V, analytically calculated, and FEM 3D simulation performed in Coventorware 153 V and 171 V respectively (shown in Table 2). Measured and simulation pull-in voltage showed better agreement within 3.5 % compared to analytically modelled which is due to 1-D analytical beam model limitations discussed in section II. Experienced pull-in voltage of demonstrated MEMS varactor is comparable to the pull-in voltage reported by Ramadoss et al for MEMS based electronically steerable antenna [7]. The pull-in voltage can be reduced using thinner copper foil for beam structures. Here we used 40 μm to ease the manual handling of the membrane. Measured tuning ratio of the MEMS varactor is 1.36, whereas modelled tuning ratio is 1.5. Therefore measurements showed close agreement with modelled tuning ratio within 9.3 %. The difference in measured and predicted displacement is due to rough surface of microwave laminate board copper clad. Measured peak to peak surface roughness of copper clad is $\sim 6 \mu\text{m}$.

Table 2. Comparison in pull-in voltages.

	Pull-in voltage (V)
Measured (V)	177
Coventorware simulation (V)	171
Analytically modelled pull in (V)	153

4.2. Resonant Frequency of the Beams

Resonant frequency measurements are carried out using LDV. From LDV measurements of deflection magnitude with respect to frequency shown in Fig. 14, in which beam deflection is measured for frequency range of 0-10 kHz. It is observed that measured resonant frequency is 2.8 kHz. Beam resonant frequency is analytically evaluated using expression 5, which is 3.23 kHz. Therefore measured and modelled resonant frequencies are in agreement within 13.5 %.

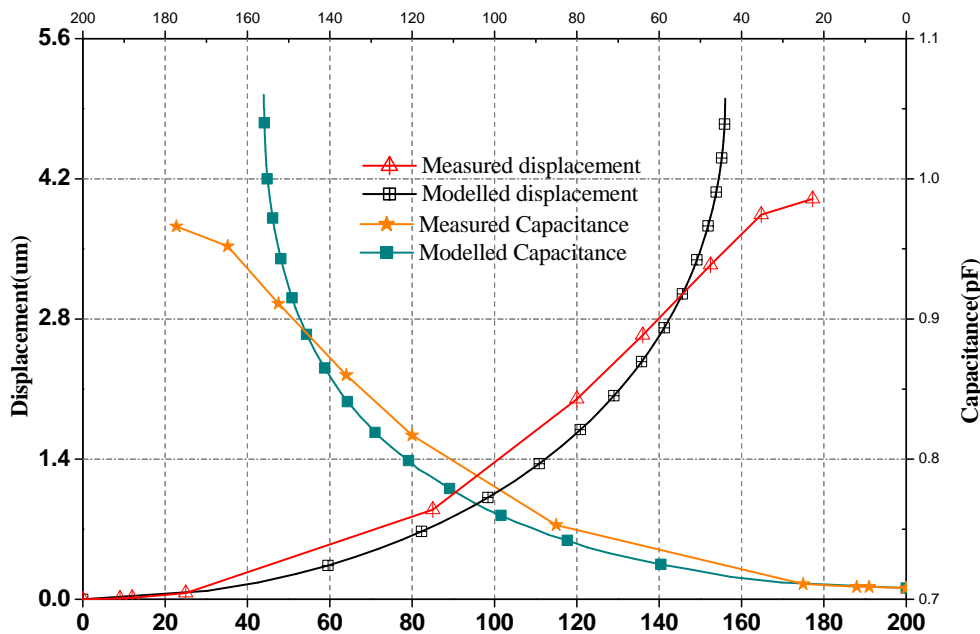


Fig. 13. Comparison in analytically modelled and measured voltage vs. displacement.

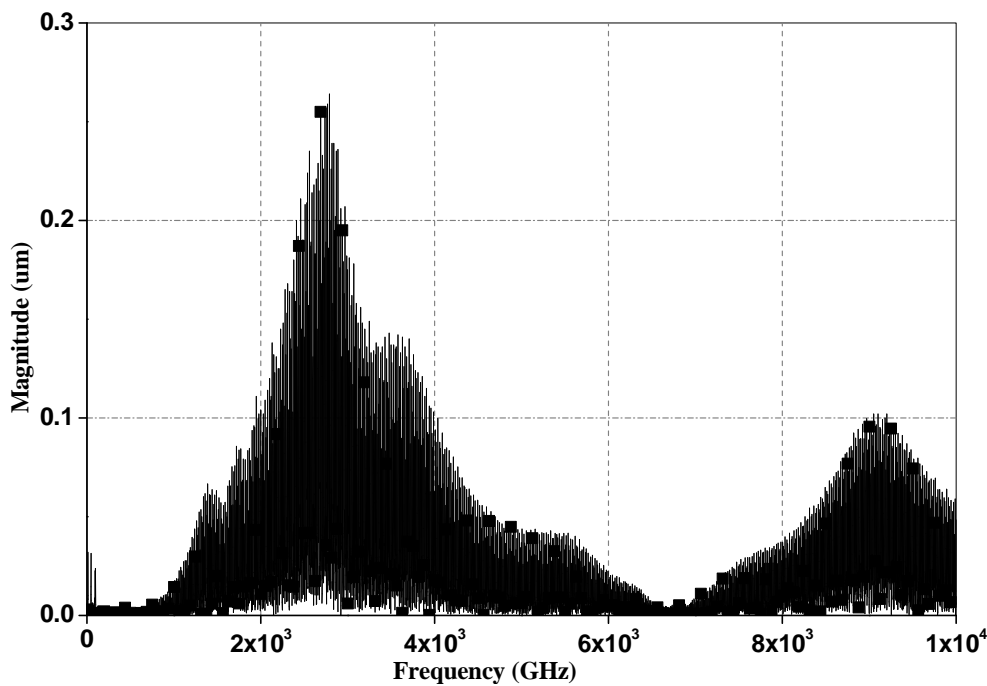


Fig. 14. LDV resonant frequency characteristics.

5. Summary

This paper demonstrates the development of an electrostatically actuated MEMS varactor on microwave laminate board for monolithic RF systems using modern PCB fabrication technology without using clean room and sophisticated fabrication equipments. The main purpose is to demonstrate the fabrication approach developed to realize RF MEMS. MEMS varacor is implemented to validate the concept. Measured and predicted characteristics of beam showed good agreement. Although the pull-in voltage of demonstrated MEMS varactor is high but it can be easily reduced using

thinner metal foil, or using multilayer membrane consist of thin metal with low Young's modulus polymer. There are beam structures such as crab leg, meandered arms to attain low pull-in voltage. Secondly, buck converter can be used to step-up voltage. This MEMS varactor can be used in distributed MEMS transmission lines for RF applications to implement phase shifter, filter, and tunable antenna on microwave laminate. This approach can be used to realize MEMS devices on unconventional substrates such as printed circuit board, low temperature cofired ceramics, liquid crystal polymers (LCP).

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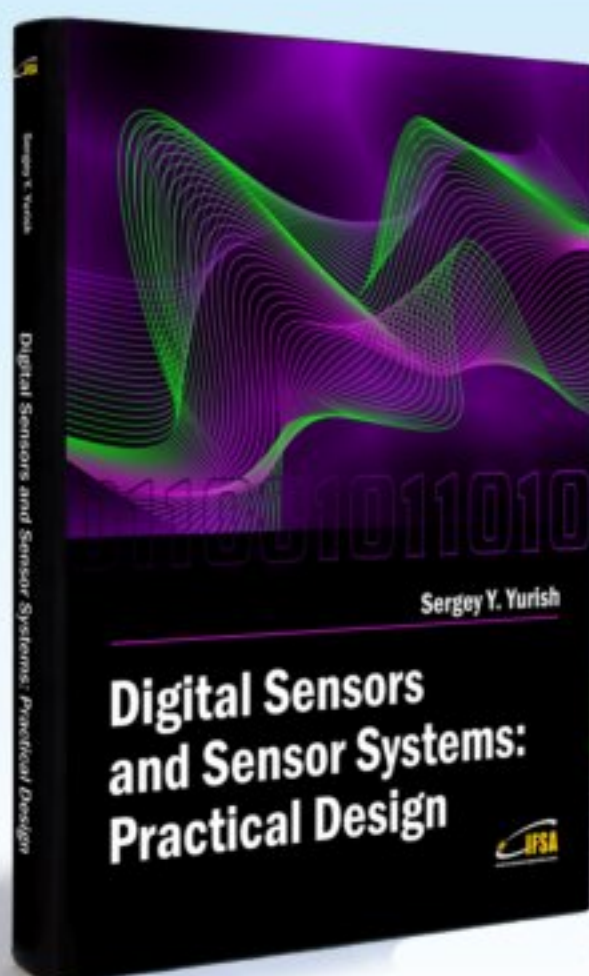
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